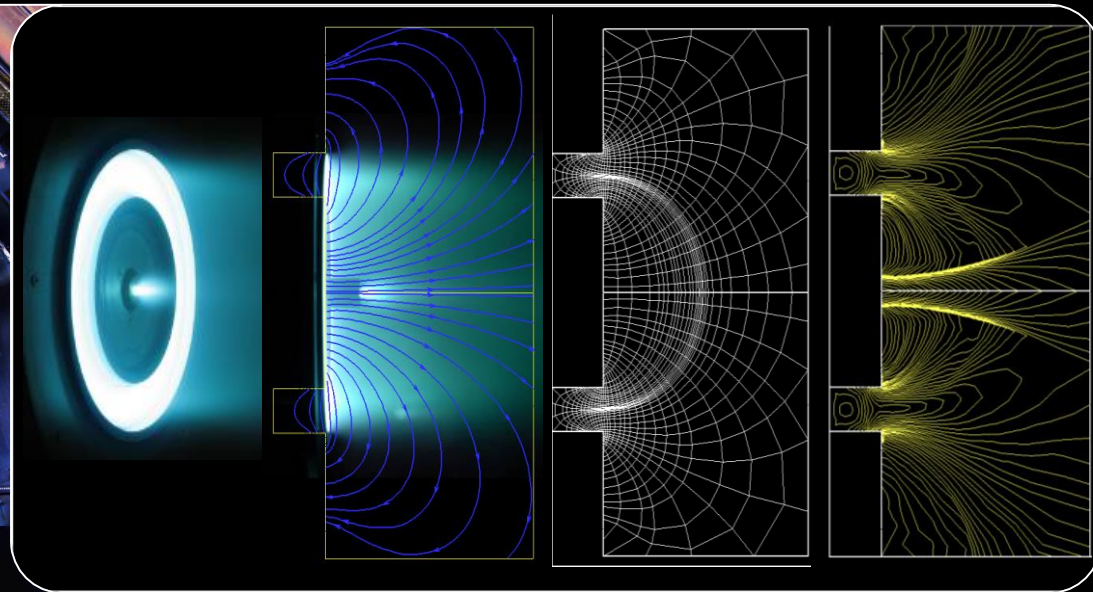
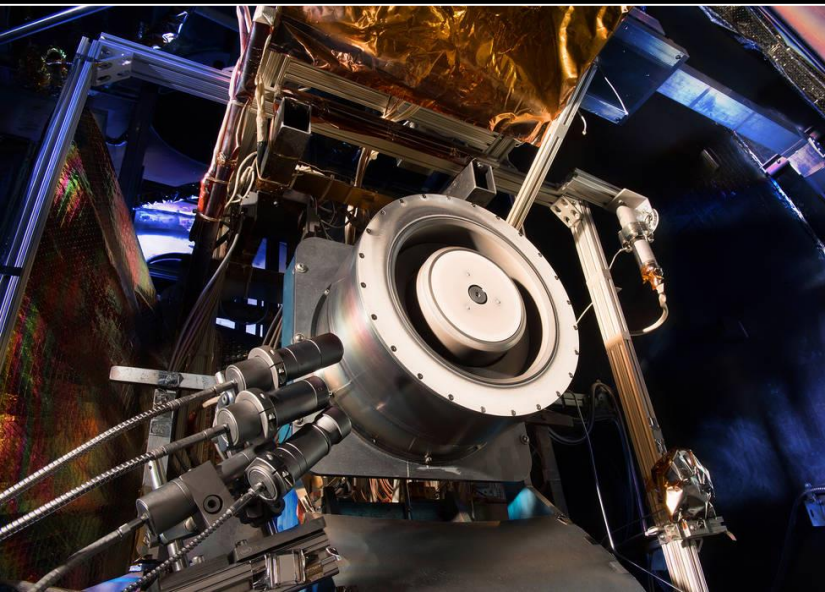




Progress on fluid computations of Hall thrusters: first-principles model for anomalous transport and dynamics effects

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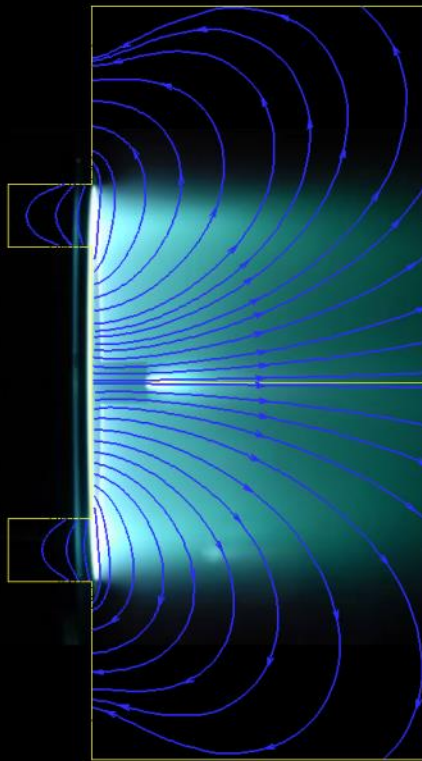


The 2-D axisymmetric (r-z) Code Hall2De

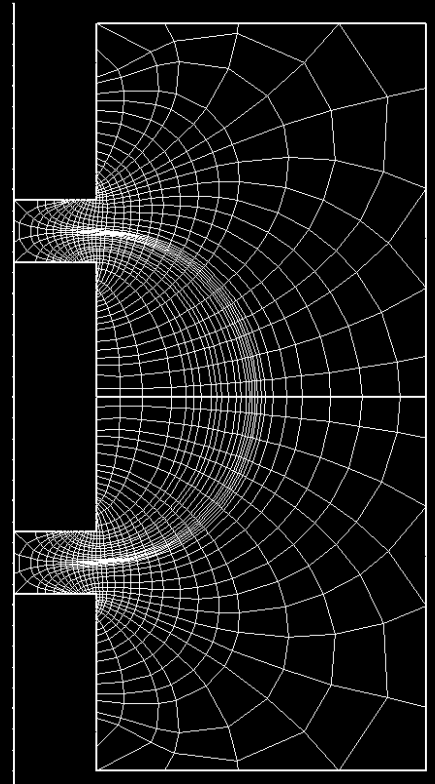
- Began development at JPL in 2008
- Discretization of all conservation laws on a magnetic field-aligned mesh
- Two components of the electron current density field accounted for in Ohm's law
- No statistical noise in the numerical solution of the heavy-species conservation laws
- Multiple ion populations allowed
- Large computational domain, extending several times the thruster channel length



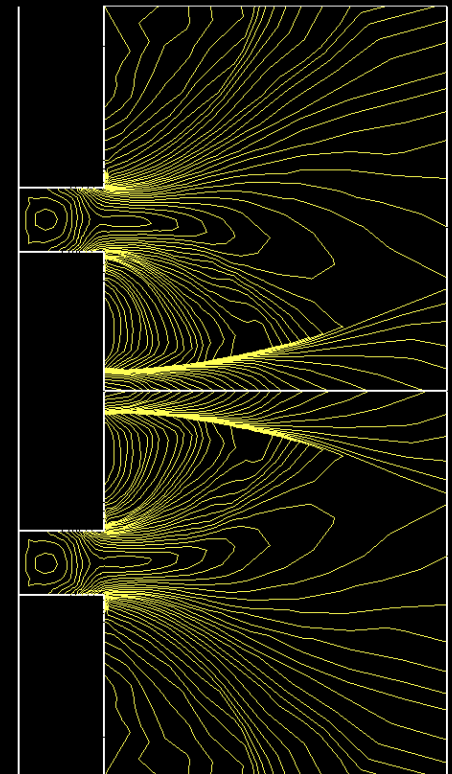
6 kW Lab Hall thruster



Magnetic field streamlines



Hall2De computational mesh



Ion density line contours



Summary

- Can a first-principles model for the anomalous transport in electrons in Hall thrusters be successfully implemented in a fluid code?
- Can a fluid code predict low frequency dynamics (i.e., breathing mode oscillations)? How sensitive these oscillations are to models (i.e., wall losses, anomalous transport, thermal conductivity)?

$$\frac{\partial n_i}{\partial t} + \nabla \cdot (n \mathbf{u})_i = \dot{n}_i, \quad \dot{n}_i = \int (f_i)_c d\mathbf{v} \Big|_{\text{inelastic}}$$

$$\frac{\partial}{\partial t} (n m \mathbf{u})_i + \nabla \cdot (n m \mathbf{u} \mathbf{u})_i = q_i n_i \mathbf{E} - \nabla p_i + \mathbf{R}_i$$

$$\mathbf{R}_i \approx - \sum_{s \neq i} n_i m_i v_{is} (\mathbf{u}_i - \mathbf{u}_s) + \int m_i \mathbf{v} (f_i)_c d\mathbf{v} \Big|_{\text{inelastic}}$$

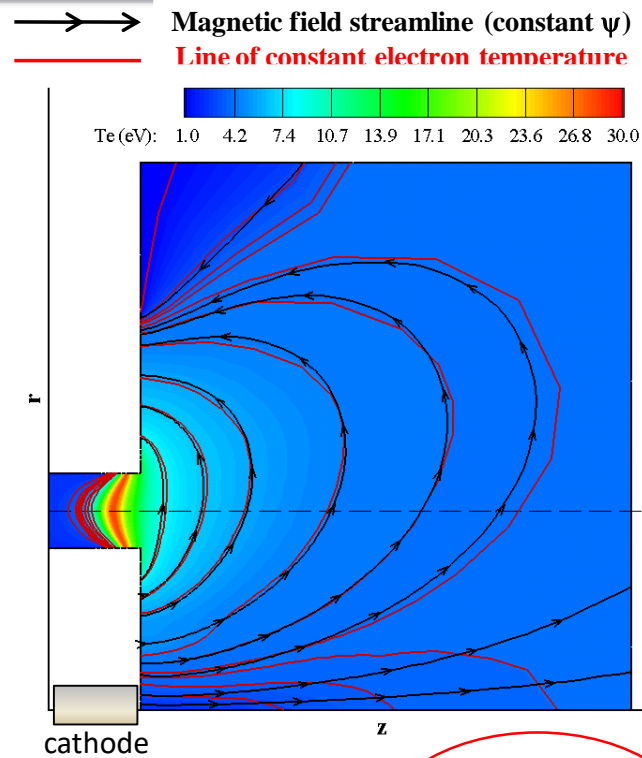
$$\nabla \cdot (\mathbf{j}_e + \mathbf{j}_i) = 0$$

$$n_e m_e \frac{D\mathbf{u}_e}{Dt} = -en_e (\mathbf{E} + \mathbf{u}_e \times \mathbf{B}) - \nabla p_e + \mathbf{R}_e$$

$$\rightarrow E_{\parallel} = \eta j_{e\parallel} - \frac{\nabla_{\parallel} p_e}{en_e} + \eta_{ei} \bar{j}_{i\parallel}, \quad E_{\perp} = \eta (1 + \Omega_e^2) j_{e\perp} - \frac{\nabla_{\perp} p_e}{en_e} + \eta_{ei} \bar{j}_{i\perp}$$

$$\eta \equiv \frac{m_e (v_c + v_a)}{e^2 n_e}$$

$$\frac{3}{2} en_e \frac{\partial T_e}{\partial t} = \mathbf{E} \cdot \mathbf{j}_e + \nabla \cdot \left(\frac{5}{2} T_e \mathbf{j}_e + \boldsymbol{\kappa}_e \cdot \nabla T_e \right) - \frac{3}{2} T_e \nabla \cdot \mathbf{j}_e - \sum_s n_e \left(\varepsilon + \frac{3}{2} T_e \right) + Q_e^T$$



- Model tracks “wave action” as representative quantity of wave magnitude
- Maximum wave action established by saturation value
- Relationship between wave action and anomalous collision frequency is non-linear in region where electrons are not Maxwellian (Fig. 1)
- **Floor** value of anomalous collision frequency assumed in non-Maxwellian regions: minimum anomalous collision frequency for which electron drift velocity < electron thermal speed (Fig. 2)

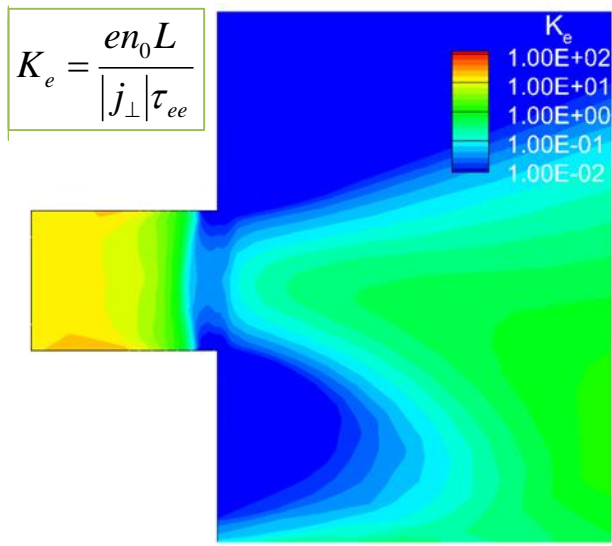


Fig. 1: For $K_e \ll 1$, electrons are not Maxwellian

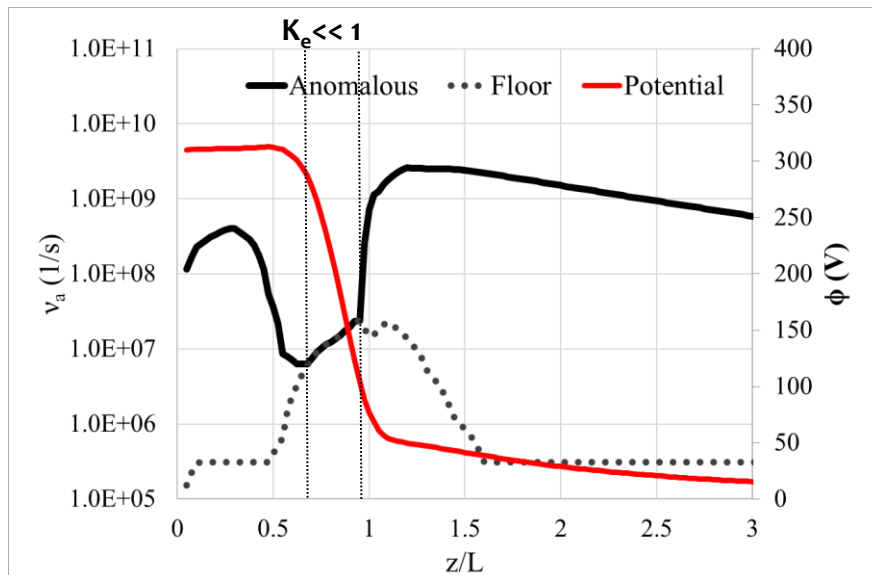
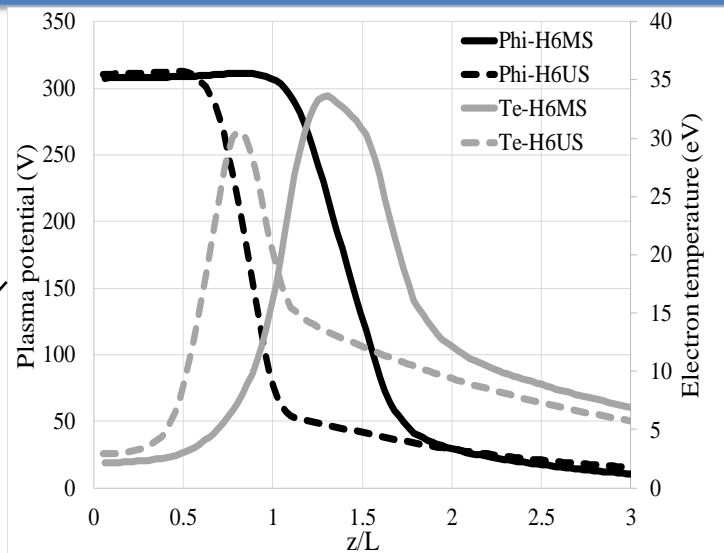


Fig. 2: Anomalous collision frequency predicted by first principles model

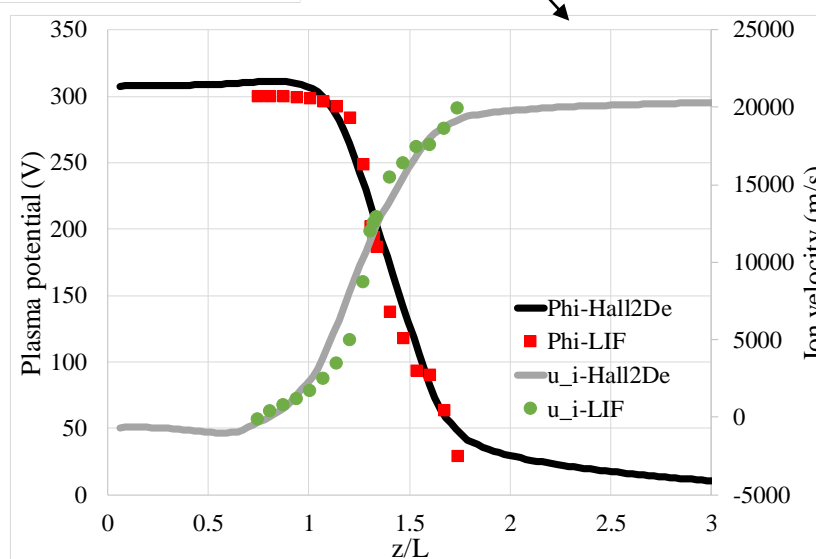
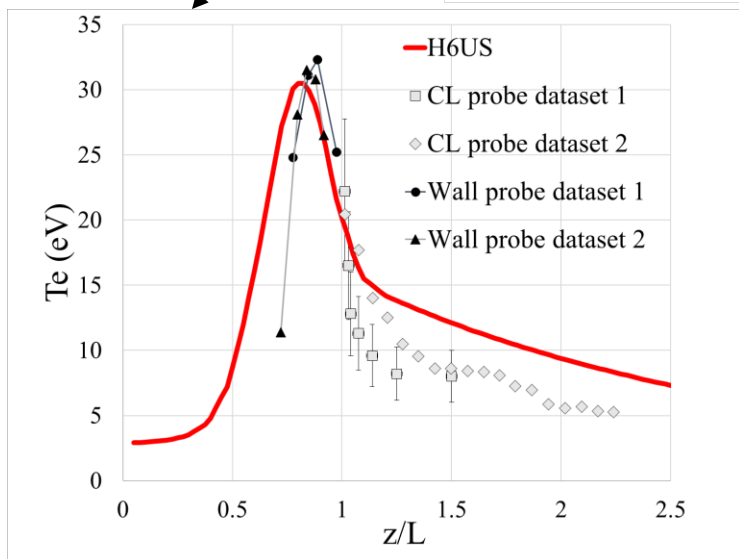


Can the first-principles model be applied successfully to multiple thrusters?

H6US comparison with experiments



H6MS comparison with experiments



Lopez Ortega et al., "Application of a first-principles anomalous transport model for electrons to multiple Hall thrusters and operating conditions", JPC 2018

Lopez Ortega et al., "A first-principles model based on saturation of the electron cyclotron drift instability for electron transport in hydrodynamics simulations of Hall thruster plasmas", IEPC 2017



Can a fluid code capture low frequency oscillations?

- We use a 1-D version of Hall2De to gain insight on low frequency oscillations
- Linearized system of equations using mass conservation of ions and neutrals produces criterion for positive growth rate

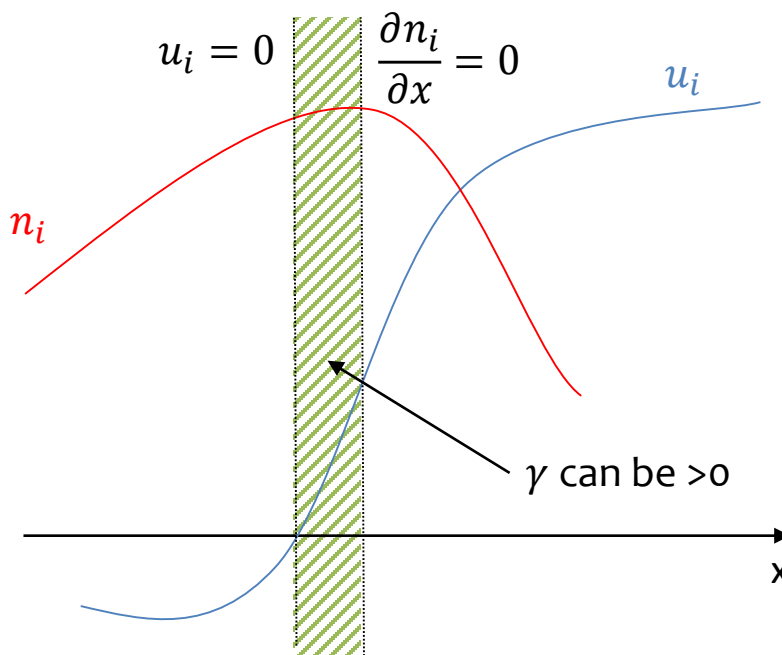
Growth rate

$$\gamma = \frac{1}{2} \left(\frac{u_i \frac{\partial n_i}{\partial x}}{n_i} + \frac{u_n \frac{\partial n_n}{\partial x}}{n_n} - \frac{\Gamma_i n_i}{n_n} \right)$$

Ion velocity (points to u_i)
 Neutral velocity (points to u_n)
 Wall loss frequency for ions (points to Γ_i)
 Ion density (points to n_i)
 Neutral density (points to n_n)

Always < 0

Must be positive for $\gamma > 0$



Assuming oscillations are small, the 0-th order steady-state solution for ion conservation can be written as:

$$\frac{u_i \frac{\partial n_i}{\partial x}}{n_i} = \underbrace{-\frac{\partial u_i}{\partial x}}_{\text{convection}} - \underbrace{\Gamma_i + c_e \sigma(T_e) n_n}_{\text{ionization}}$$

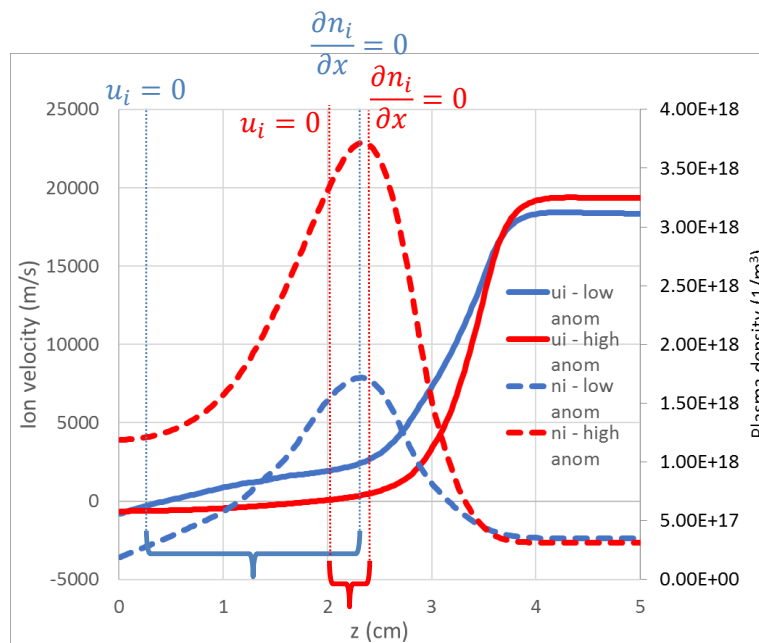
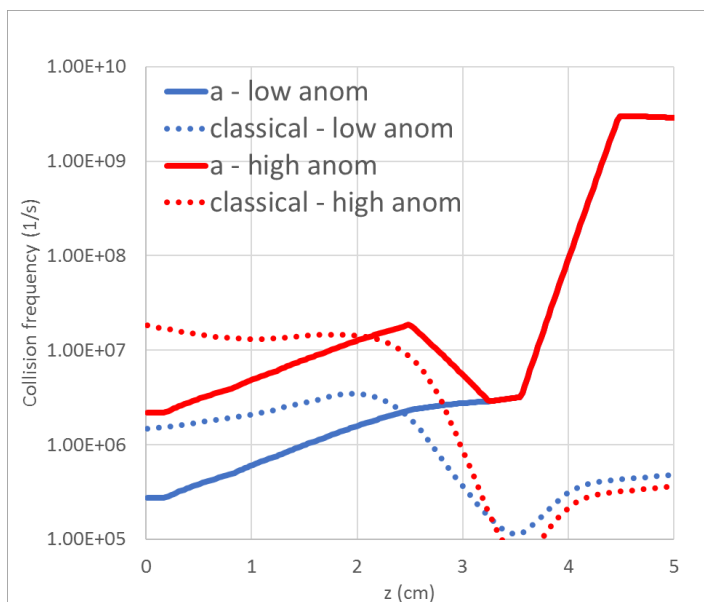
convection < ionization



Can a fluid code capture low frequency oscillations? What drives them?

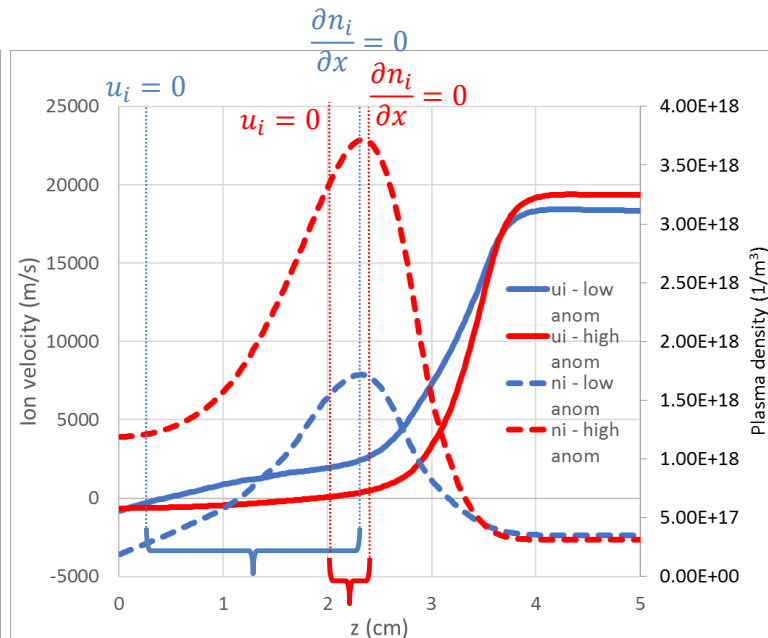
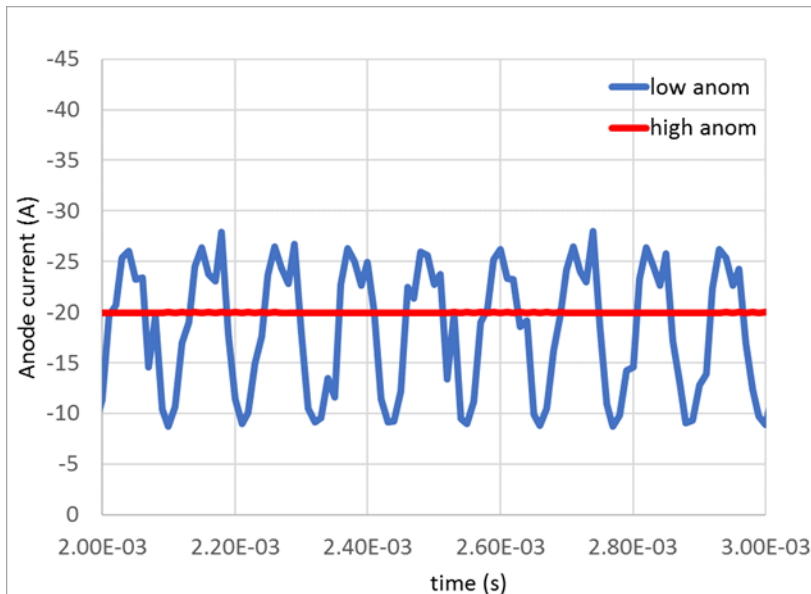
- Presence of oscillations is very sensitive to small changes in models that produce reasonable plasma solutions:
 - Wall losses
 - Thermal conductivity
 - Collision cross sections
 - Ionization cross sections
 - Anomalous collision frequency

Example: anomalous collision frequency



- Presence of oscillations is very sensitive to small changes in models that produce reasonable plasma solutions:
 - Wall losses
 - Thermal conductivity
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 - Ionization cross sections
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Example: anomalous collision frequency





BACK UP





Major assumptions of first-principles model

$$\frac{\partial N_k}{\partial t} + \mathbf{u}_i \cdot \nabla N_k = 2\omega_{i,k,linear} \left(1 - \frac{N_k}{N_{k,sat}} \right)$$

Includes electron drift + Landau damping

$$N_{k,sat} = \frac{n_0 T_e}{4nc_s(1 + k^2 \lambda_{De}^2)}$$

Limits plasma potential oscillations not to exceed T_e

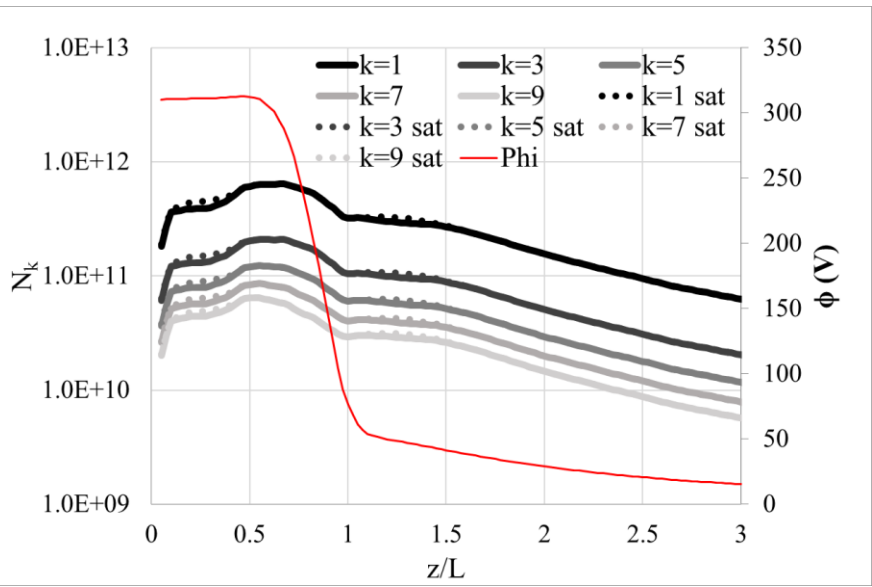
$$v_a = \frac{2e}{Nm_e n_0 |\mathbf{u}_e - \mathbf{u}_i|} \sum_k k N_k \omega_{ie,k,nonlinear}$$

Number of discrete wavenumbers

Includes electron drift

$$K_e \gg 1 \quad \omega_{ie,k,nonlinear} = \omega_{ie,k,linear}$$

$$K_e \ll 1 \quad \omega_{ie,k,nonlinear} ??$$



$$K_e = \frac{en_0 L}{|j_{\perp}| \tau_{ee}}$$

$$\frac{\partial N_k}{\partial t} + \mathbf{u}_i \cdot \nabla N_k = 2\omega_{i,k,linear} \left(1 - \frac{N_k}{N_{k,sat}} \right)$$



Can a fluid code capture low frequency oscillations?

Linearized system with analytical solution: ion density + neutral density equations in 1-D

$$\frac{Dn_i}{Dt} = -n_i \frac{\partial u_i}{\partial x} + \underbrace{kn_i n_n}_{\text{ionization}} - \underbrace{\Gamma_i n_i}_{\text{wall losses}}$$

→ steady state

$$u_i \frac{\partial n_i}{\partial x} = -n_i \frac{\partial u_i}{\partial x} + kn_i n_n - \Gamma_i n_i$$

$$\frac{Dn_n}{Dt} = -kn_i n_n + \Gamma_i n_i$$

linearized system

$$u_n \frac{\partial n_n}{\partial x} = -kn_i n_n + \Gamma_i n_i$$

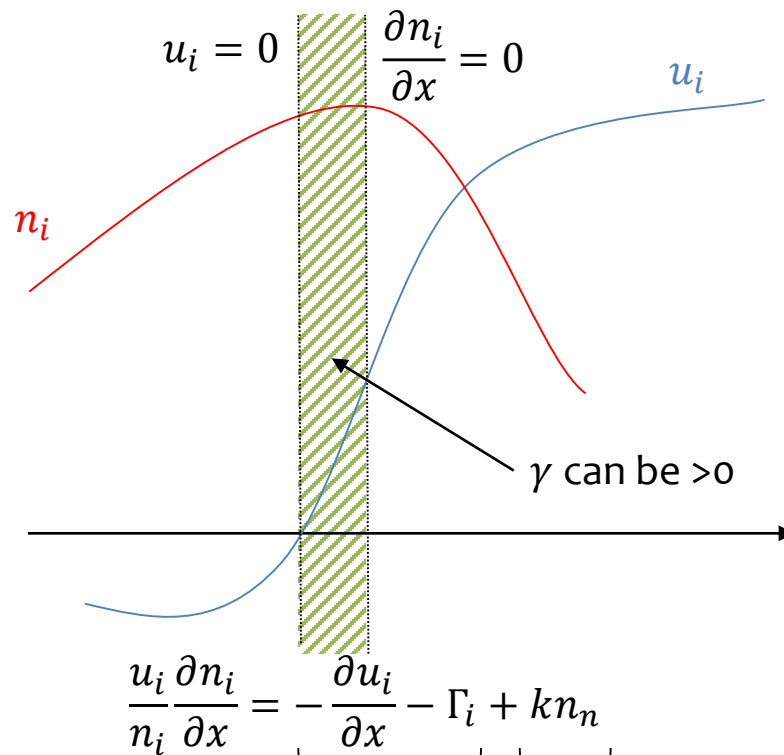
$$\frac{D}{Dt} \begin{pmatrix} n'_i \\ n'_n \end{pmatrix} = \begin{bmatrix} -\frac{\partial u_i}{\partial x} + kn_n - \Gamma_i & kn_i \\ -kn_n + \Gamma_i & -kn_i \end{bmatrix} \begin{pmatrix} n'_i \\ n'_n \end{pmatrix} = 0$$

Growth rate

$$\gamma = \frac{1}{2} \left(\underbrace{\frac{u_i \partial n_i}{n_i \partial x}}_{\text{boxed}} + \underbrace{\frac{u_n \partial n_n}{n_n \partial x} - \frac{\Gamma_i n_i}{n_n}}_{< 0} \right)$$

Frequency

$$\omega^2 = kn_i \frac{\partial u_i}{\partial x} - \gamma^2$$



convection < ionization